

AZIPOD USER GROUP, 2017-14-06

Shaftline Bearing lifetime calculation

Background

Sami Palokangas, Azipod® X/V Technology Manager

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Azipod® bearing arrangement and affecting forces

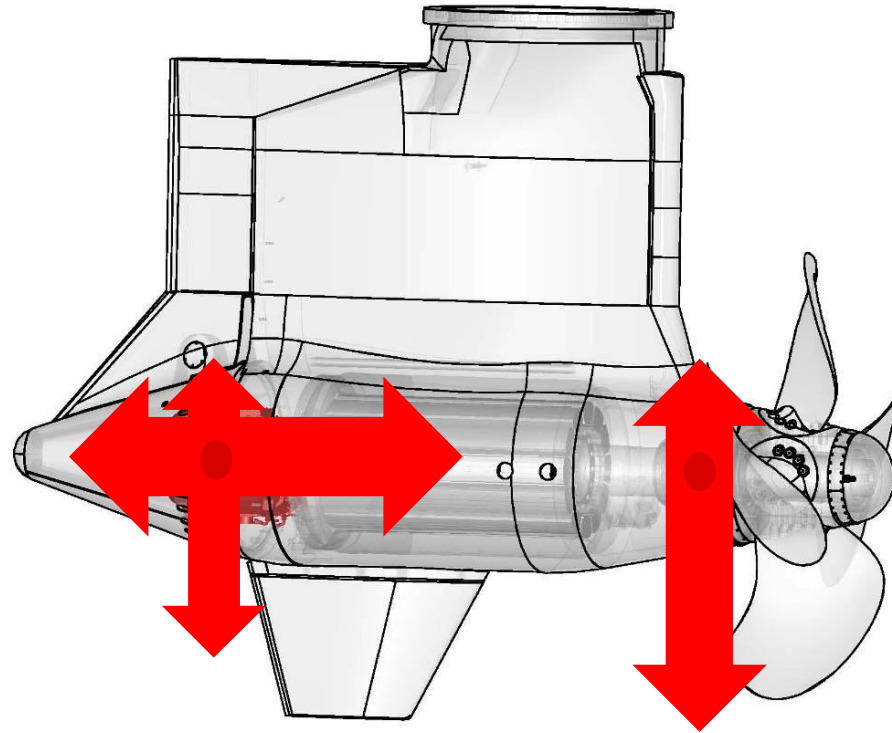
NDE-Bearing

Axial Forces

- Propeller Thrust force

Radial Forces

- Shaftline weight
- Magnetic pull
- (Propeller side forces)

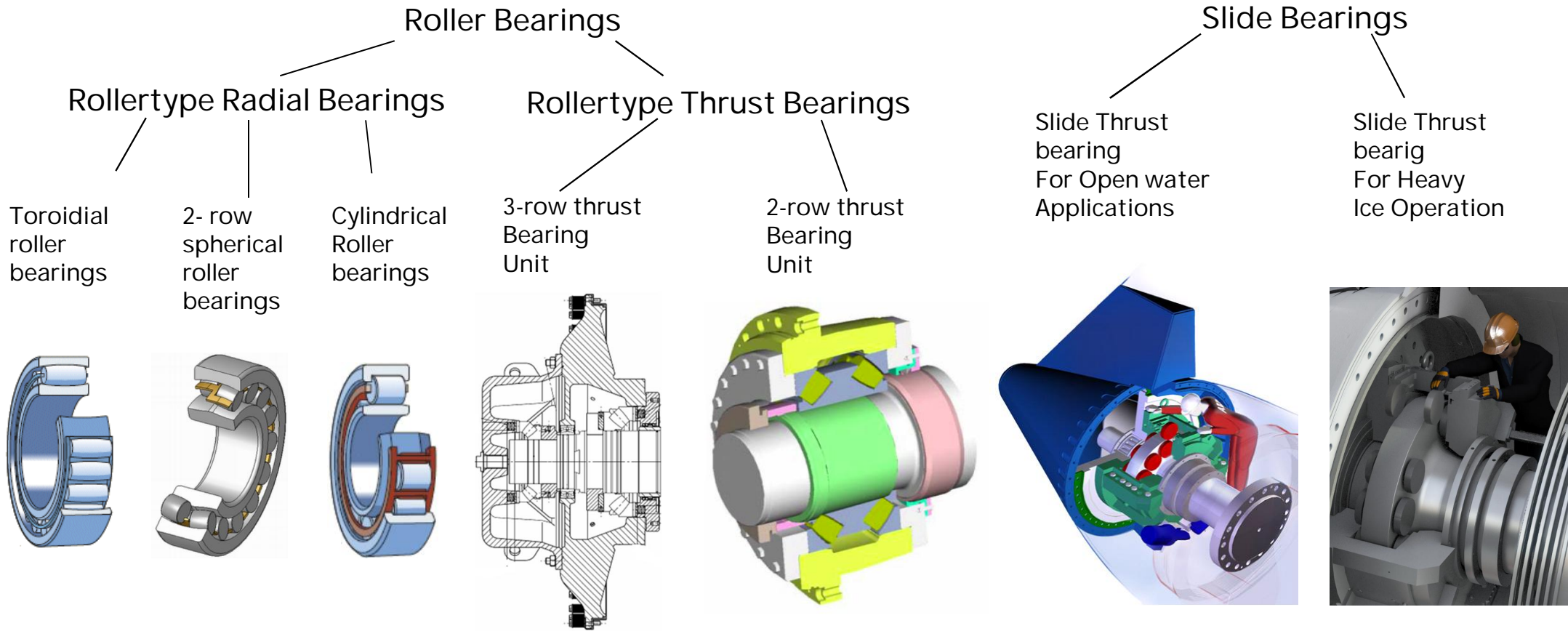


DE Eng Bearing

Radial Forces

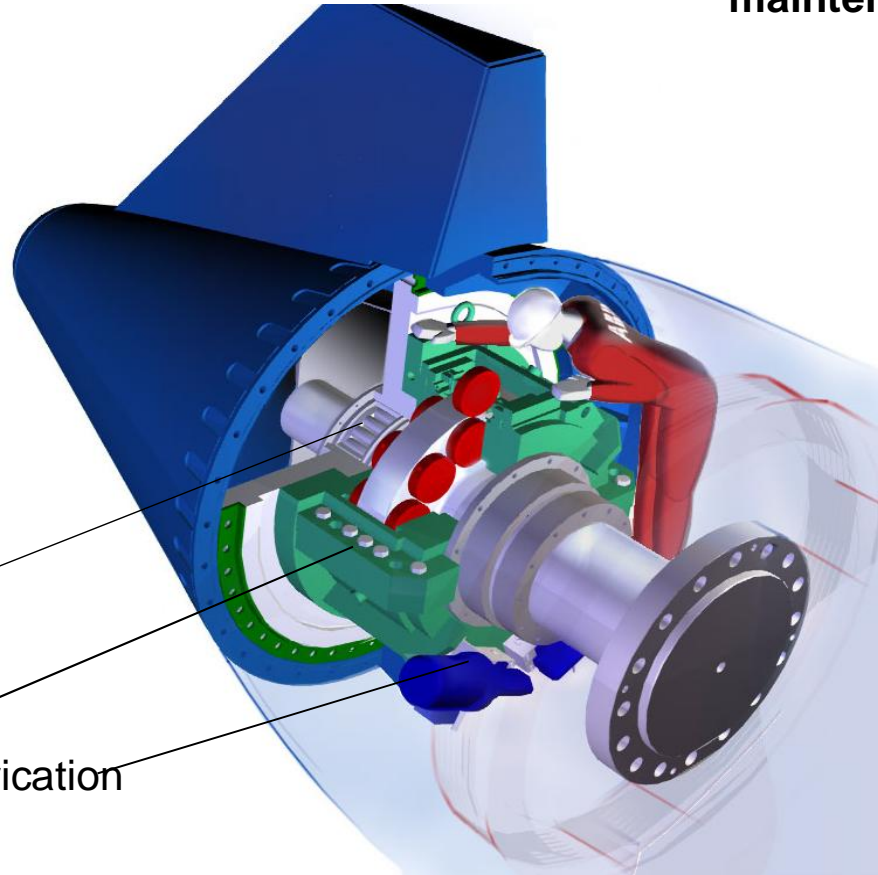
- Shaftline weight
- Propeller side forces
- Magnetic pull

Azipod® Bearing types



Hybrid thrust bearing concept

Designed to be robust with **minimum maintenance cost**



Well known and proven Technologies:

Non-drive-end radial **roller** bearing

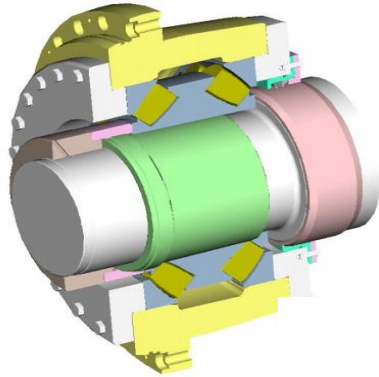
Slide thrust bearing

Redundant lubrication

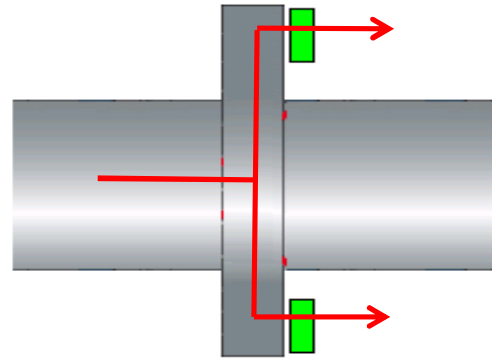
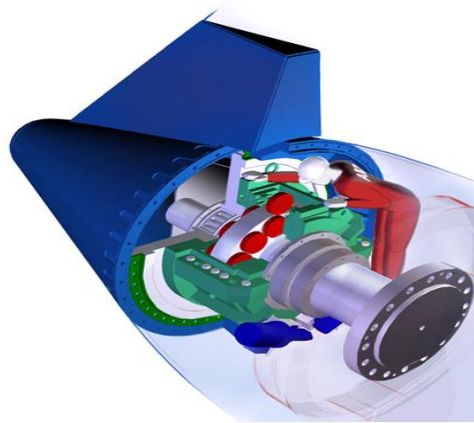
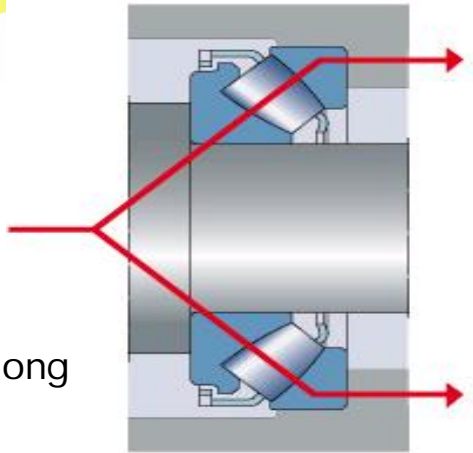
Patent pending

Thrust pad change inside Azipod unit does not require dry-docking.

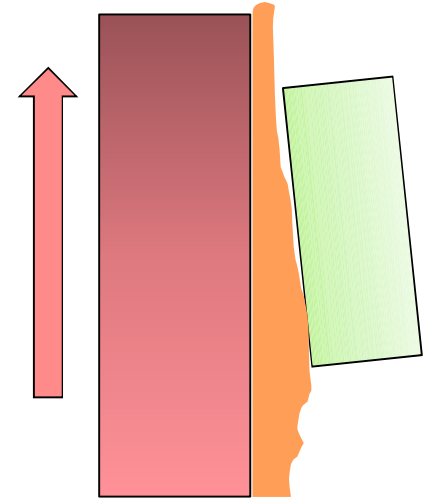
Main Features: Roller bearing vs. Slide bearing

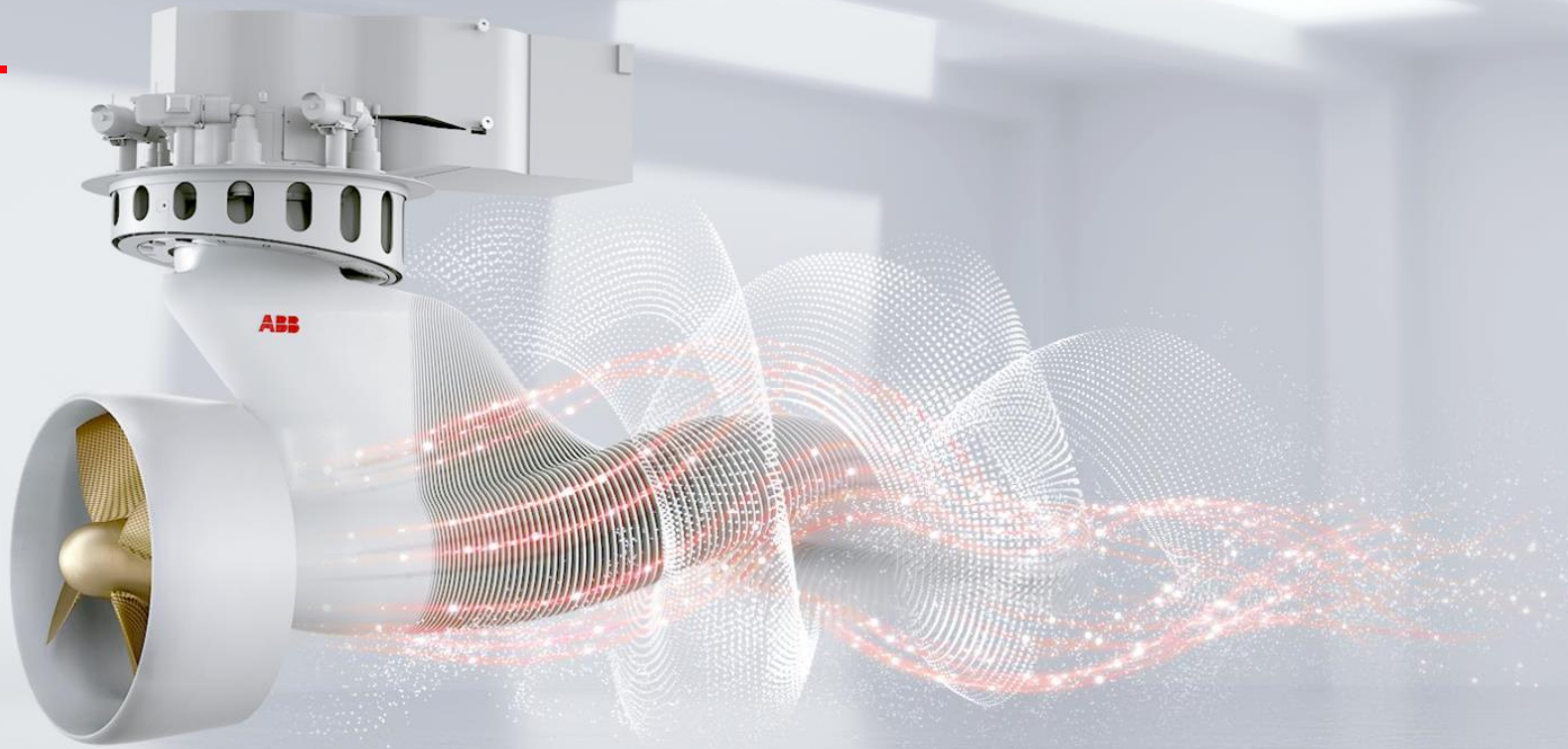


- Thin oil film
- High surface pressure
- Dimensioning based on fatigue
- Failure process can take long time
- Radial load partly carried by same bearing



- Thick oil film
- Low surface pressure
- No fatigue
- Sliding surface may damage rapidly if oil film disappears
- Radial load load carried by separate bearing





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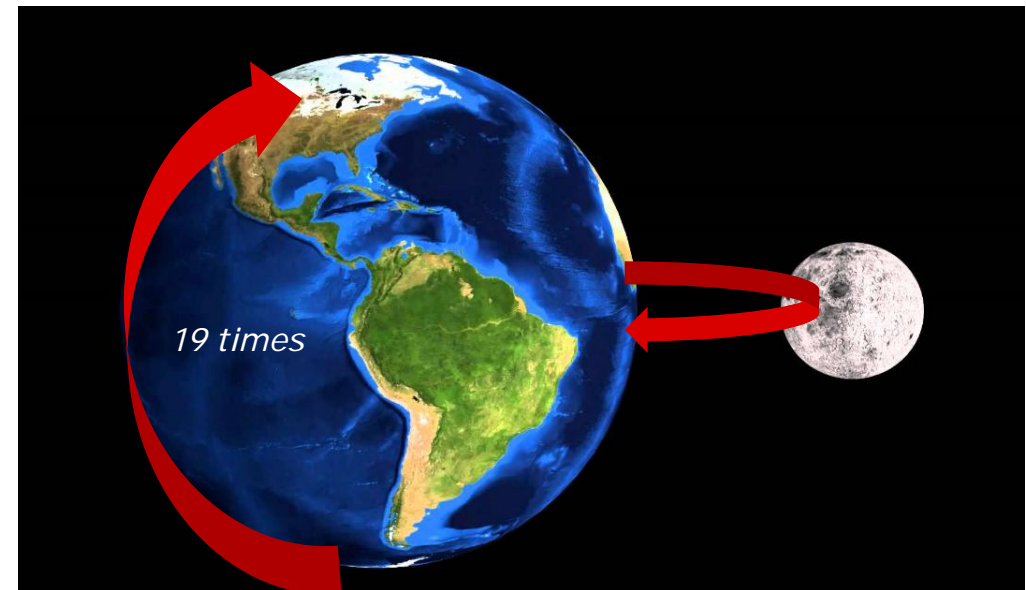
Bearing lifetime and dimensioning

Roller Bearings

Sami Palokangas, Azipod® X/V Technology Manager

Why to use roller bearings in Azipod®

- Low friction (low heat losses)
- Low start up torque
- Zero speed operation
- Wear down close to zero
 - 650mm shaft 140rpm
 - => 150 000 km relative motion per year
- Limited space available
- Reversible rotation
- High stiffness
- Low radial clearance

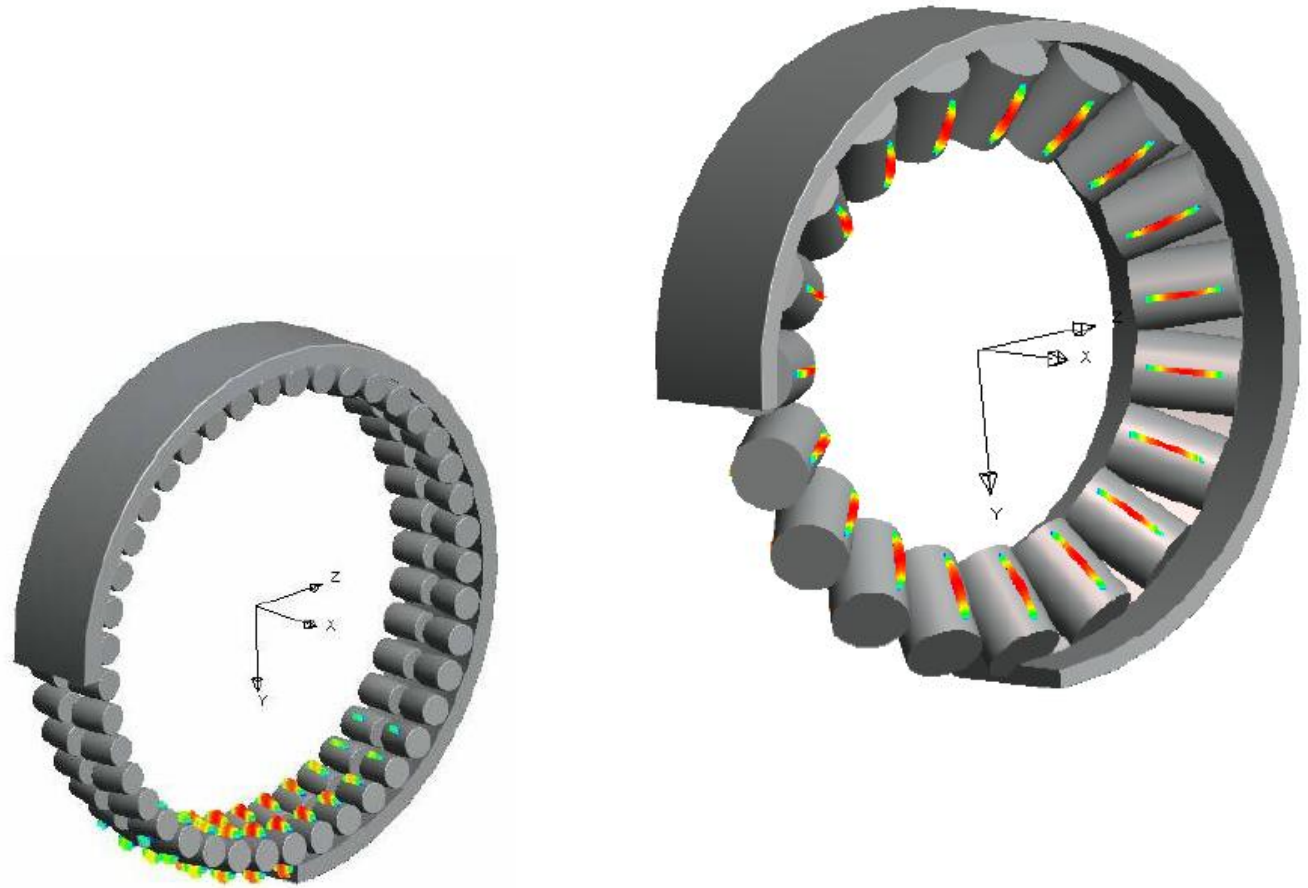


*During 5 years dry-dock interval:
To Moon and back or 19 times around the world*

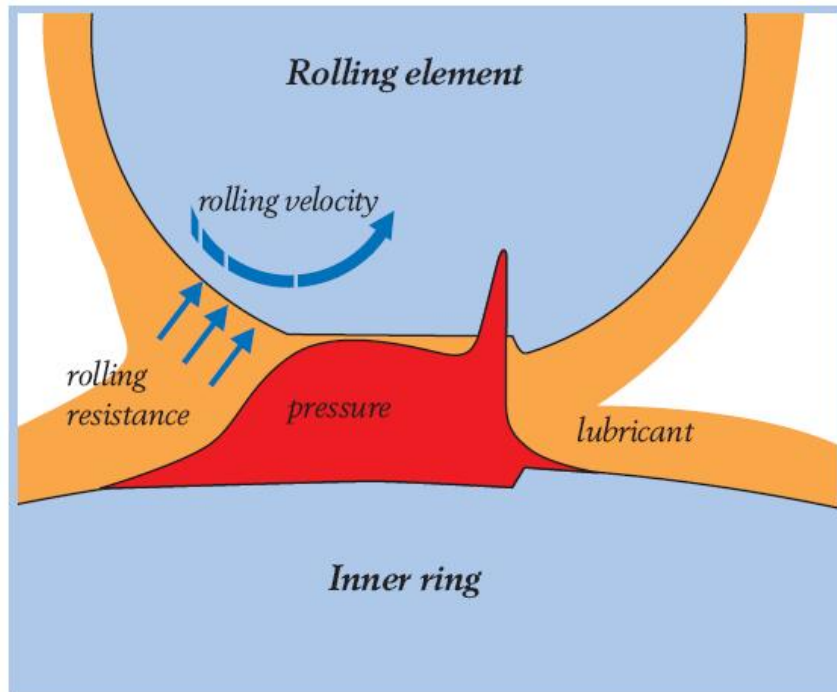
Rolling contact

Basis for Dimensioning

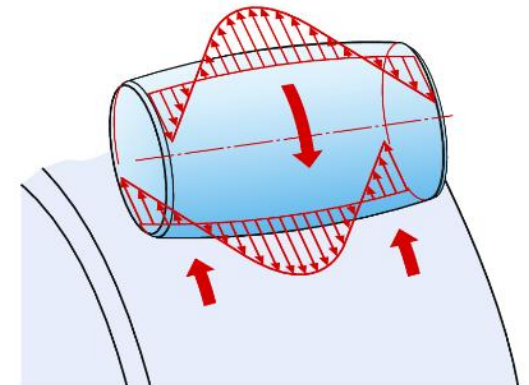
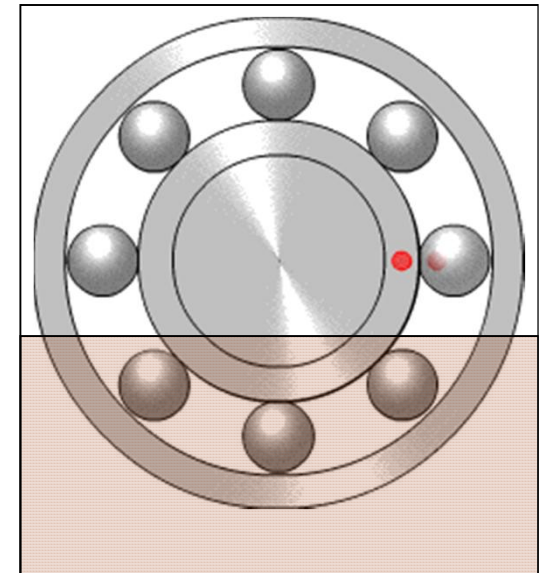
- Line contact
- Very high contact pressures
- typically 1500 MPa (\Rightarrow 15000 bar)
- High sub surface shear stress
- Lifetime calculation is based on fatigue



Elastohydrodynamic Lubrication



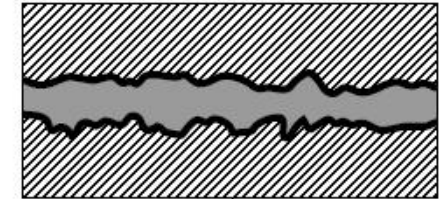
Lubricant film thickness and pressure distribution in an elastohydrodynamically lubricated contact. The large tail in the pressure at the inlet of the contact produces a resultant moment opposite to the rolling direction.



By Guillermo Morales Espejel, Tribology & Lubrication, SKF Engineering Research Centre, Nieuwegein, the Netherlands.

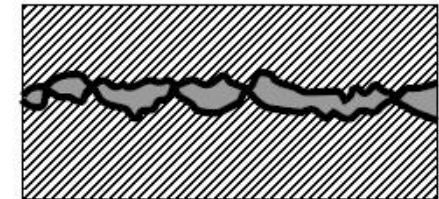
Lubrication Condition

Full fluid film lubrication: The surfaces of the components in relative motion are separated by lubricant film.



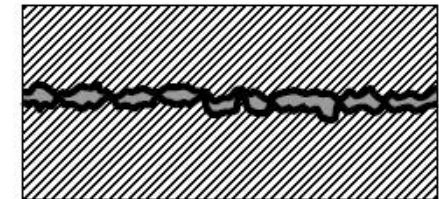
a) Full fluid film lubrication
The surfaces are completely separated by a load carrying oil film

Mixed lubrication: Where the lubricant film gets too thin, local metal-to-metal contact occurs, resulting in mixed friction.



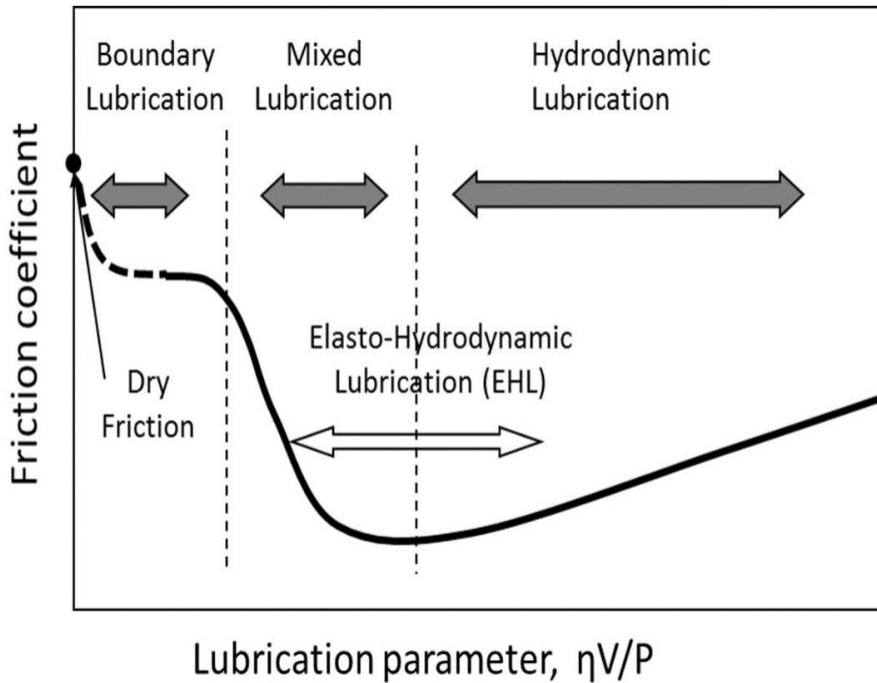
b) Mixed lubrication
Both the load carrying oil film and the boundary layer play a major role

Boundary condition: If the lubricant contains suitable additives, reactions between the additives and the metal surfaces are triggered at the high pressures and temperatures in contact areas. The resulting reaction products have a lubricating effect and form a thin boundary layer.



c) Boundary lubrication
The lubrication effect mainly depends on the lubricating properties of the boundary layer

■ Boundary layer ■ Lubricant layer



Basic bearing lifetime L10

L10 is the nominal rating life in millions of revolutions which is reached or exceeded by at least 90% of a large group of identical bearings

C = Dynamic load rating

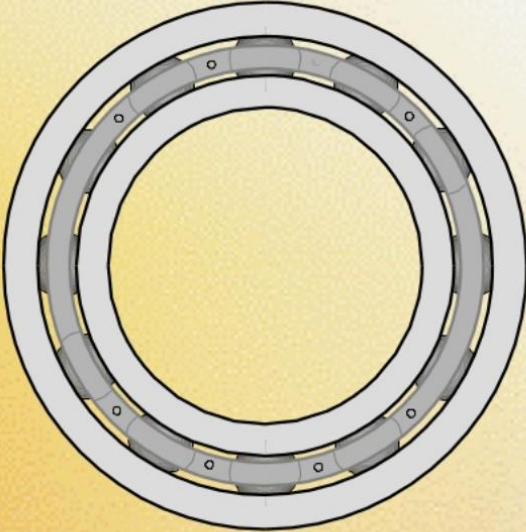
P = Equivalent dynamic load

P = Life exponent

p = 3 for ball bearings

p = 10/3 for roller bearings

Bearing Life



$$L_{10} = \left(\frac{C}{P}\right)^p \quad \text{Lundberg Palmgren Equation 1947}$$

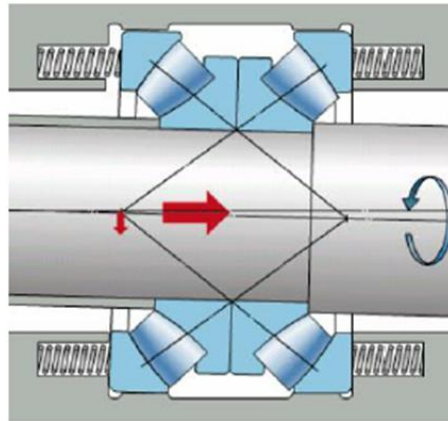
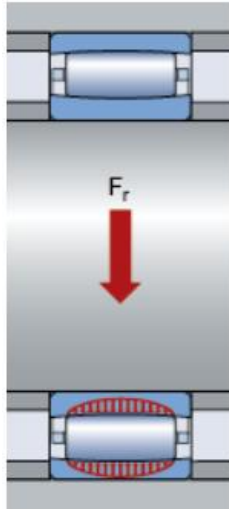
$$L_{na} = a_1 a_{23} \left(\frac{C}{P}\right)^p \quad \text{Adjusted Rating Life Equation 1977}$$

$$L_{naa} = a_1 a_{skf} \left(\frac{C}{P}\right)^p \quad \text{New SKF Life Equation 1989}$$

=> ISO 281:2007

Equivalent Dynamic Load

- In Toroidal bearings only radial force is relevant
- In Roller Thrust Bearings both Axial and Radial Forces have to be taken into consideration in dimensioning



Bearing Life

Equivalent Dynamic Bearing Load

$$P = X F_r + Y F_a$$

Where :

X = Radial Load Factor

Y = Axial Load Factor

Load Ratings

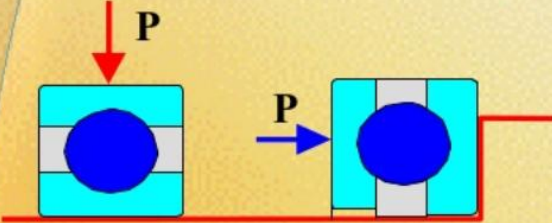
Dynamic vs. Static

Basic dynamic calculations typically define the bearing size in open water vessels.

Static safety factor is checked against shock loads, which are important dimensioning factor especially in ice operation.

Load carrying capacity

Basic dynamic load rating C



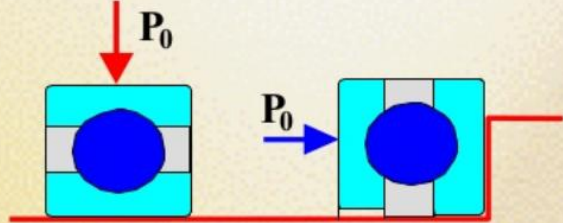
The ISO life equation

$$L_{10} = \left(\frac{C}{P}\right)^p$$

L_{10} = basic rating life, millions of revolutions
 C = basic dynamic load rating, N
 P = equivalent dynamic bearing load, N
 p = exponent of the life equation

With the load $P = C$
the L_{10} life will be 1 million revolutions

Basic static load rating C_0




The static safety factor

$$s_0 = \frac{C_0}{P_0}$$

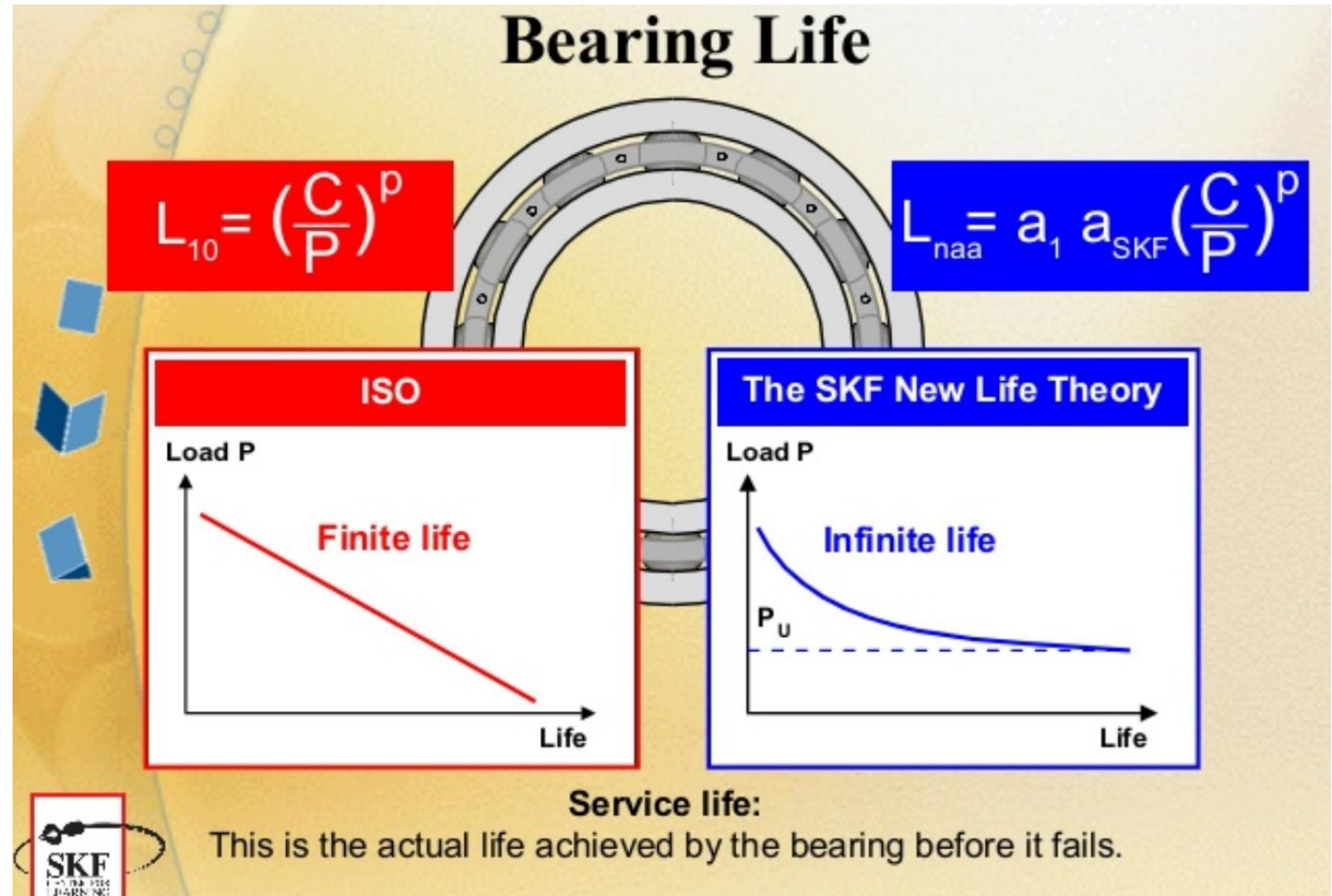
s_0 = static safety factor
 P_0 = equivalent static bearing load, N
 C_0 = basic static load rating, N

With the load $P = C_0$
the static safety factor s_0 will be 1



ISO281:2007

- Since [ISO 281](#) was published in 1990, additional knowledge has been gained regarding the influence on bearing life of contamination, lubrication, internal stresses from mounting, stresses from hardening, fatigue load limit of the material, etc
- New method takes these conditions into consideration.



Affecting factors

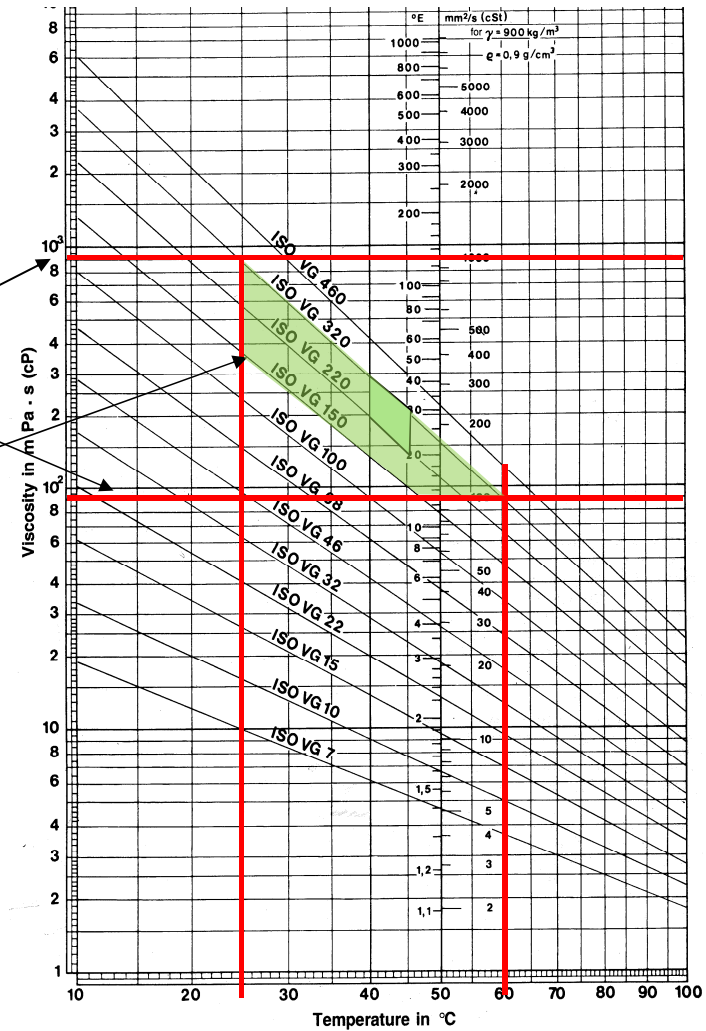
Viscosity

cSt limits 100 - 1000 mm²/s

Recommended area

Normal operating area

Temperature range 25°C - 60°C



Affecting factors

Viscosity Ratio κ (kappa)

κ tells the lubrication condition.

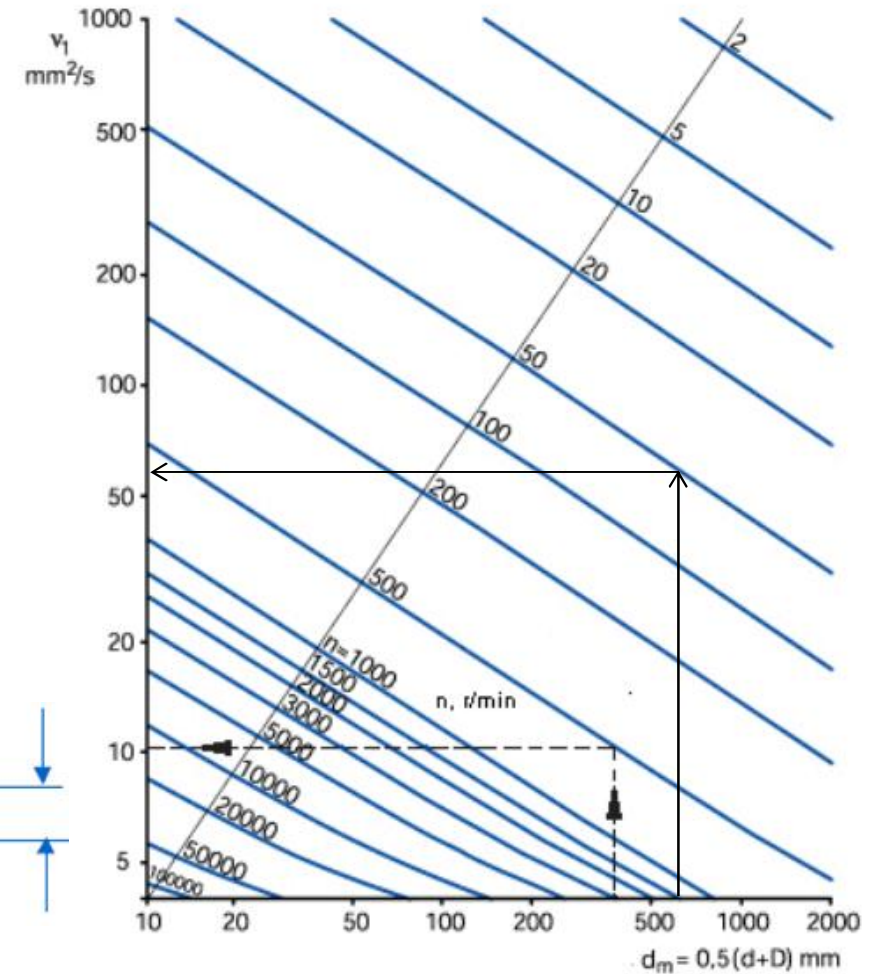
Adequate lubrication is considered when $\kappa > 1$

$$\kappa = \frac{v}{v_1}$$

κ	=	viscosity ratio
v	=	operating viscosity of the lubricant [mm ² /s]
v_1	=	rated viscosity depending on the bearing mean diameter and rotational speed [mm ² /s]



Required viscosity v_1 at operating temperature



Affecting factors

Contamination

Contamination factors for SKF bearings.

Condition	Factor η_c ¹⁾	
	for bearings with diameter $d_m < 100$	for bearings with diameter $d_m \geq 100$ mm
Extreme cleanliness Particle size of the order of the lubricant film thickness Laboratory conditions	1	1
High cleanliness Oil filtered through an extremely fine filter Conditions typical of bearings greased for life and sealed	0,8 ... 0,6	0,9 ... 0,8
Normal cleanliness Oil filtered through a fine filter Conditions typical of bearings greased for life and shielded	0,6 ... 0,5	0,8 ... 0,6
Slight contamination Slight contamination of the lubricant	0,5 ... 0,3	0,6 ... 0,4
Typical contamination Conditions typical of bearings without integral seals, coarse filtering, wear particles, and ingress from surroundings	0,3 ... 0,1	0,4 ... 0,2
Severe contamination Bearing environment heavily contaminated and bearing arrangement with inadequate sealing	0,1 ... 0	0,1 ... 0
Very severe contamination Under extreme contamination, values of η_c can be outside the scale resulting in a more severe reduction of life than predicted by the equation for L_{nm}	0	0

Affecting factors

Water content

Roller bearings are more sensitive to water than slide bearings

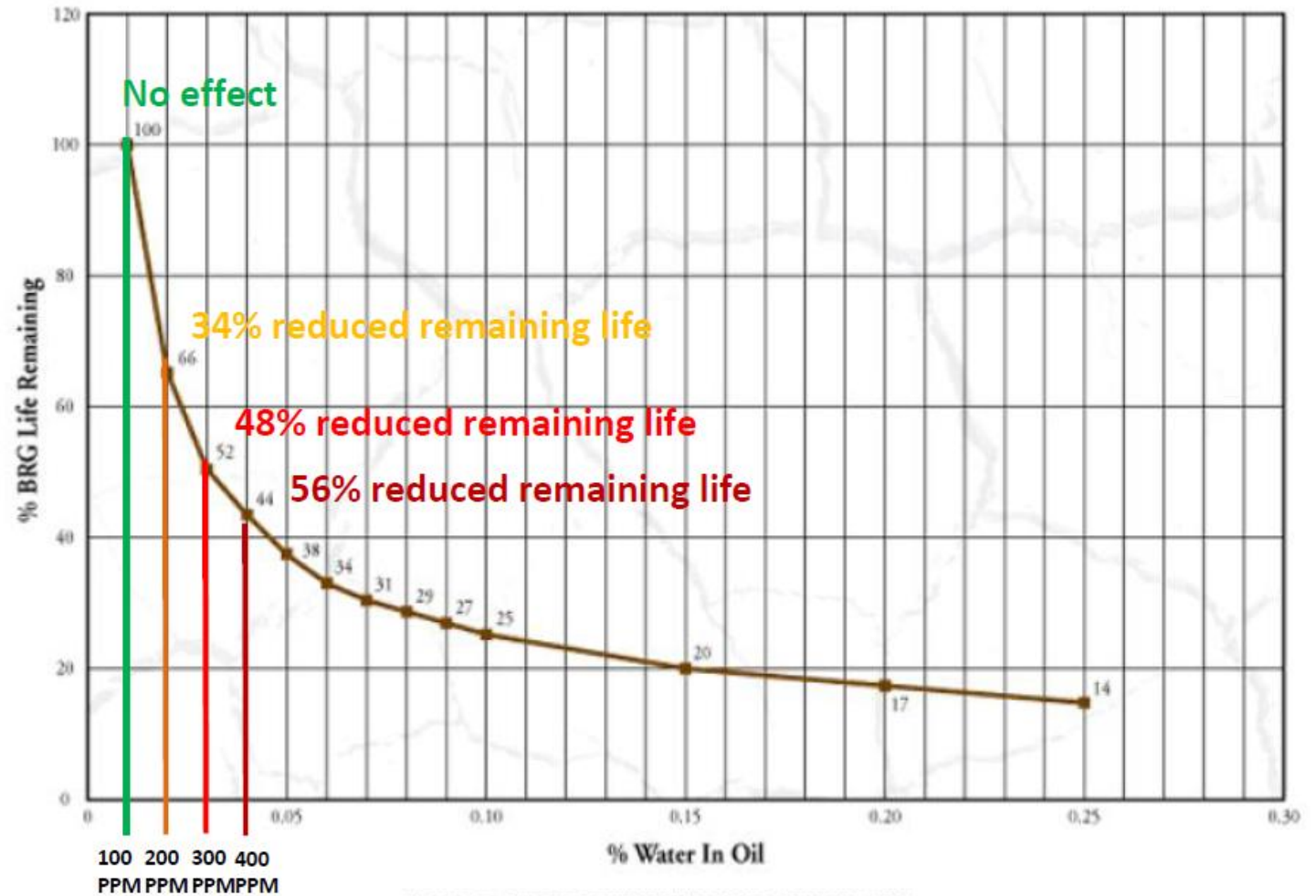
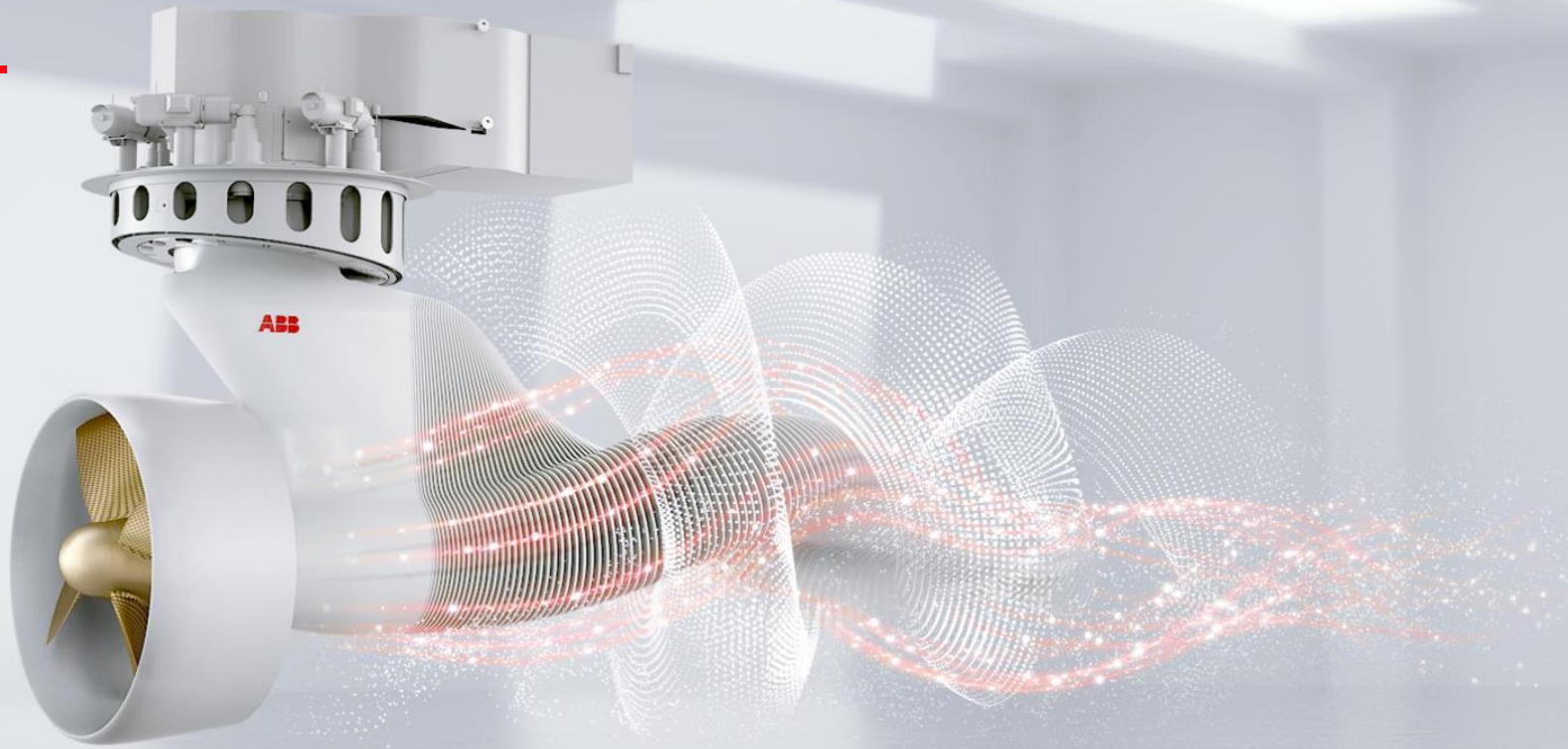


FIGURE 2. WATER CONTAMINATION VS. BEARING LIFE



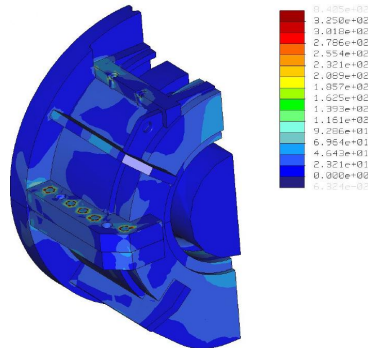
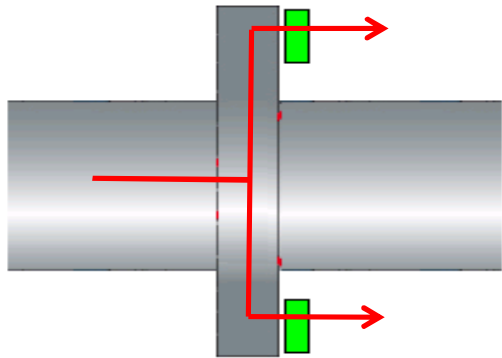
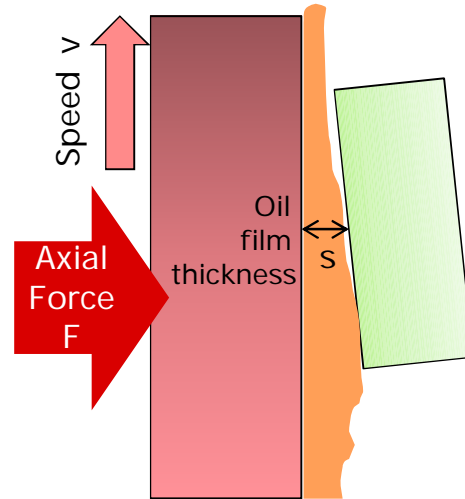
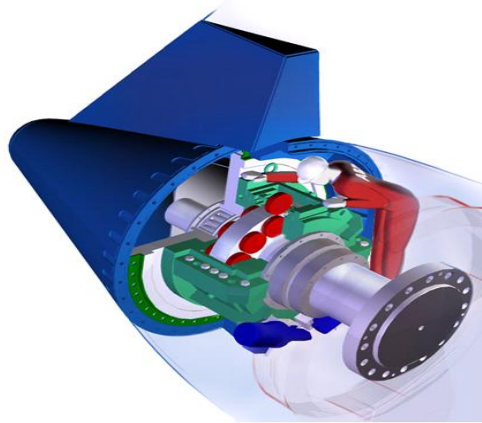
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Bearing lifetime and dimensioning

Slide Bearings

Sami Palokangas, Azipod® X/V Technology Manager

Dimensioning principle of Axial Slide bearing



Dimensioning is based on:

1. Hydrodynamic lubrication
 - As long as there is oil film between surfaces there is no wear.
 - Dimensioning has to be sufficient to ensure lubricating film in every operating condition.
2. Shock Loads & Static strength
 - Need to have enough sliding surface area to withstand compression loads from normal operation and possible shock loads.
 - All Mechanical parts of the bearing needs to withstand all loads from normal operation and also from rare special conditions.

Hydrodynamic calculation of slide thrust bearing

Start information for calculation

Green = positive effect Red = Negative effect

#	Main Input Value	Effect on oil film Thicker the better	Effect on temp. Lower the better
1	Sliding speed	Green	Red
2	Axial force by propeller	Red	Red
3	Start-up force	Red	Red
4	Oil viscosity grade	Green	Red
5	Oil IN temperature	Red	Red
6	Oil Flow	Green	Green
7	Shaft movements in dynamic situations	Red	Red

Hydrodynamic calculation

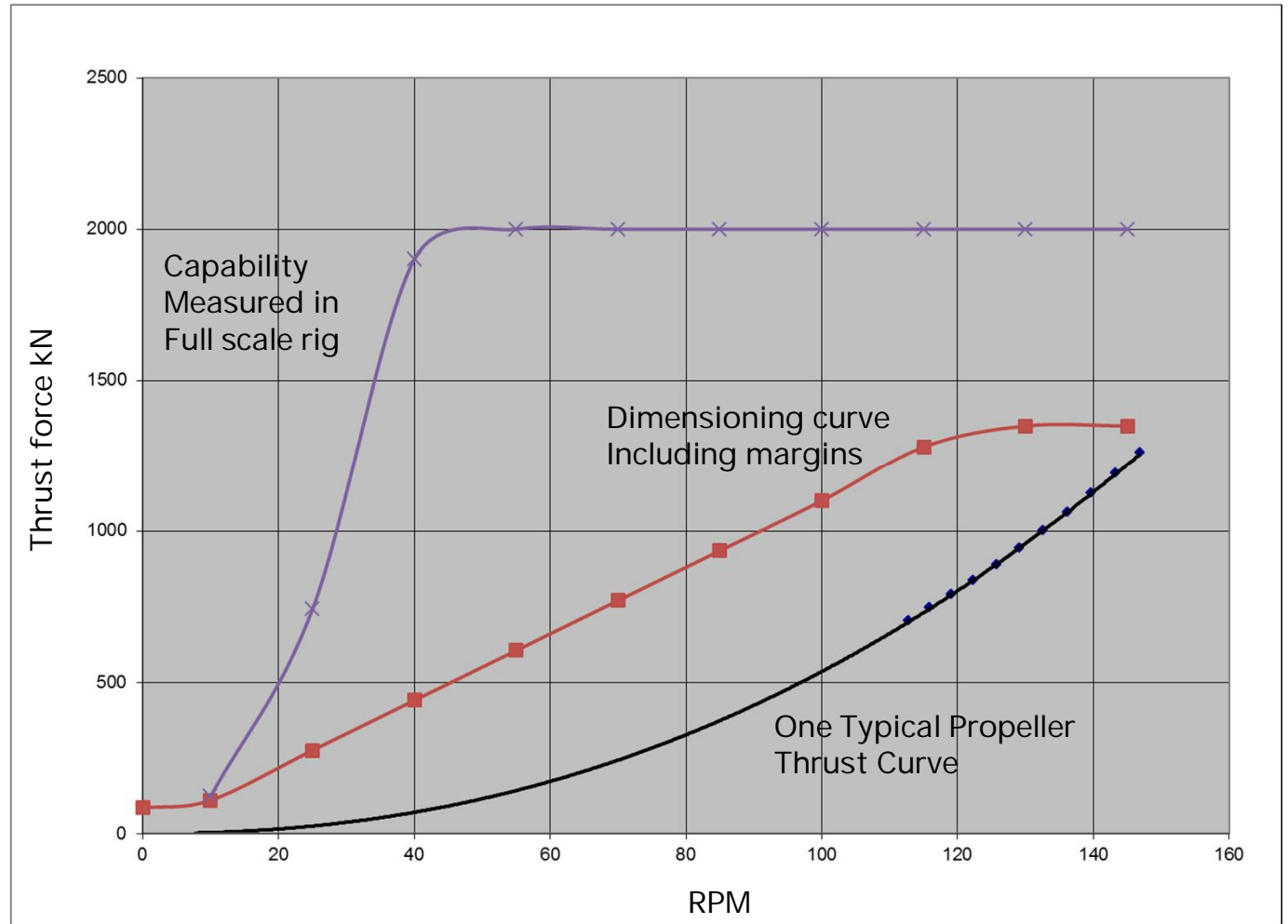
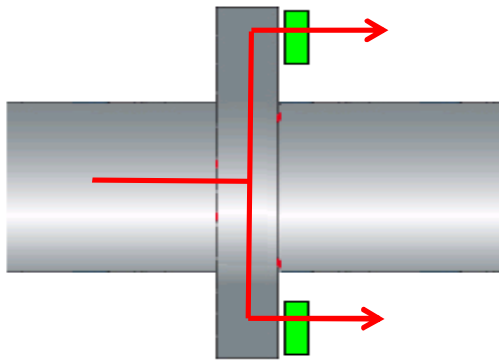
The image shows a technical data sheet for a hydrodynamic calculation of a slide thrust bearing. The document is in German and contains the following information:

- Header:** Includes the title 'Hydrodynamische Berechnung von Gleitlagerungen' and a reference to 'ABB 2.3 1974'.
- Input Data:** Lists various parameters such as bearing diameter, length, and oil viscosity, with their respective units and values.
- Operating Conditions:** Provides details about the operating speed, axial force, and other relevant factors.
- Results:** Displays calculated values for oil film thickness, temperature, and other performance metrics.
- Notes:** Contains explanatory text regarding the calculation method and assumptions.

Axial slide bearing

Dimensioning

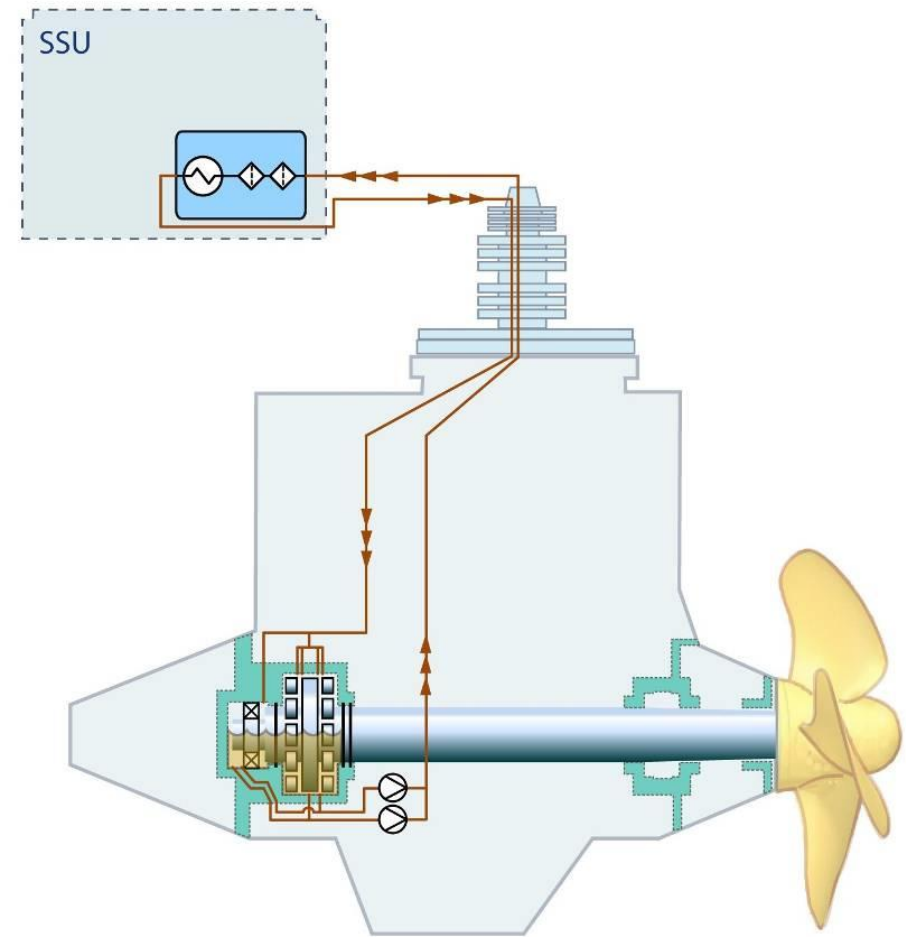
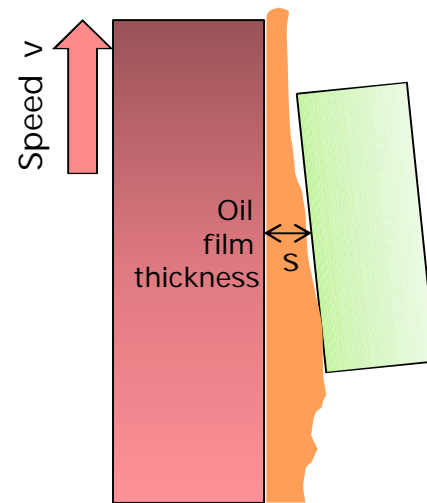
Dimensioning vs. measured performance



Affecting factors

Hybrid Thrust Bearing Unit

- Rolling bearing oil film thickness is typically $0.2-1\ \mu\text{m}$
- In slide bearing the oil film thickness is typically $20-30\ \mu\text{m}$: more robust against contamination and water content
- In ABB Hybrid Thrust bearing unit, roller bearing and slide bearing utilize same oil and same oil circulation. Therefore the roller bearing defines the cleanliness and water content requirement.
- However, also in slide bearing particles can cause scratches on sliding surface.





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